

# Halbach Girder Fabrication Integration Meeting



Attendees: S. Peggs, D. Trbojevic, S. Berg, G. Mahler, S. Brooks, S. Trabocchi, T. Roser, N. Tsoupas, J. Tuozzolo

Minutes 1/11/17 meeting

1. The permanent magnet material (PMM) blocks order was placed by procurement. Delivery is estimated as March 17, need an update from the vendor.
2. N. Tsoupas presented the corrector study results. It was agreed that the quad and dipole corrector specifications (slide 11) were adequate and provided reasonable margin. The quad corrector provides field adjustment if Halbach field shimming strength leveling does not meet its goal. The present plan is to build the correctors with quad windings; but, not to install quad power supplies until proved necessary by production Halbach magnet measurement results. This should be a project risk list item.
3. The dipole strength provides lattice tuning and correction capability. While the dipole strength was approved there are still some on-going lattice studies.
4. It was agreed that the dipoles and quads should be separate windings. There was extended discussion on the benefit of matching the resistance of the corrector types. It was noted by R. Lambiase that the higher power needed to drive the quad correction (6x dipole correction if the same wire size is used) would at least double the power supply cost.
5. The corrector's inside dimensions work well with the present Halbach design.
6. N. Tsoupas will do a final iteration on the coil winding design and provide the information to S. Trabocchi for engineering design. Schedule is tight the fabrication drawings for the steel are needed ASAP.
7. A thermal analysis needs to be done (S. Trabocchi) to provide a better estimate of the heat that will transferred from the correctors to the Halbach magnet. This is required to provide specifications to Cornell for the water stabilization system (heat load, flow rate, pressure drop).
8. G. Mahler presented the latest results (attached below) of the deflection analysis for the split Halbach magnet designs using a vertical split. The dipole (BD) had the largest displacement, .0051" (slide 23) because of the offset nature of the block installation. S. Brooks confirmed that was ok. The quad (QF) was not an issue because of the balanced frame thickness, deflection was <.0003" (slide 21).
9. George presented the latest results of the thermal analysis for temperature stabilizing of the Halbach permanent magnet material (PMM) for both QF and BD designs. The analysis is still very conservative assuming 100% of the heat from the corrector coils at max. current was on the surface of the frame. The analysis showed that water cooling could effectively stabilize the temperature of the permanent magnet material with optimized (reduced number) of water passages. The split frame clamping bolts need to be added to the model.
10. There was discussion on the PMM block shimming method to balance the magnet to magnet field strength. The present frame design allows for shimming the blocks by 0.1 to 0.8 mm (.004 to .031"). The PMM blocks for the preproduction magnets were purchased with 2% higher strength to put them in the middle of the shim range and within the 2% tolerance specification for the material. There was discussion on the method for same testing PPM for field strength. Methode will be needed for production material QA assistance testing and defining the shimming requirements.
11. Schedule is tight, George was tasked with developing a fabrication drawing for the aluminum frames ASAP. Starting without the water passages so material (aluminum plate) can be ordered and fabrication<sup>1</sup>can be planned.

# Critical Project Dates

## Technical milestones (NYSERDA contract Table 2)

| # Milestone   | Date               |                             |
|---|--------------------|-----------------------------|
| NYSERDA funding start date  | 2016 Oct 31        |                             |
| 1 Engineering design documentation complete                           | 2017 Feb 1         |                             |
| 2 Prototype girder assembled  | 2017 May 1         |                             |
| 3 Magnet production approved  | 2017 July 1        |                             |
| 4 <b>Beam through Main Linac Cryomodule</b>                           | <b>2017 Sept 1</b> | <b>CRITICAL: Go/no go 1</b> |
| 5 First arc production magnet tested                                  | 2018 Jan 1         |                             |
| 6 <b>Fractional Arc Test: beam through MLC &amp; prototype girder</b> | <b>2018 May 1</b>  | <b>CRITICAL: Go/no go 2</b> |
| 7 Girder production run complete                                      | 2018 Dec 1         |                             |
| 8 Final assembly & pre-beam commissioning complete                    | 2019 Mar 1         |                             |
| 9 Single pass beam energy scan  | 2019 July 1        |                             |
| 10 Single pass beam with energy recovery                              | 2019 Nov 1         |                             |
| 11 Four pass beam with energy recovery (low current)                  | 2020 Jan 1         |                             |
| 12 C-Beta commissioned and project complete                           | 2020 May 1         |                             |

*Engineering design documentation complete*                      *Feb 1, 2017*

*1<sup>st</sup> Article QF and QD Magnets assembled and tested* *May 1, 2017*

Prototype Girder Assembled                      May 1, 2017

Magnet production plan                      April 1, 2017

Magnet production approved                      July 1, 2017

# 1<sup>st</sup> Halibach Priorities

Build and magnetically measure 8 preproduction halbach magnets w/8 correctors

1. **Order PMM for 5 + 5 magnets + 1+ 1 for margin. S. Brooks, G. Mahler**
2. **Design QF halbach split aluminum frames – Design, order. Mahler, Trabocchi**  
**Deflection analysis complete. Mahler**  
**Water cooling/stabilization passages/thermal and analysis. Mahler**  
**Fabrication drawing, order. Mahler, designer?**
3. **Magnetic strength shimming method. Mahler, Brooks**
4. **Define and design halbach inner tuning steel wire holder – order**  
Define Brooks, Design/Fab Mahler/Trabocchi
5. Test plan for permanent magnet material to determine magnetic strength and orientation: shimming dimension. Brooks
6. Repeat 1 through 4 for BD



# 1<sup>st</sup> Correctors Priorities

Build and magnetically measure 8 preproduction halbach magnets w/8 correctors

1. Define and design correctors – order steel cores, wire.

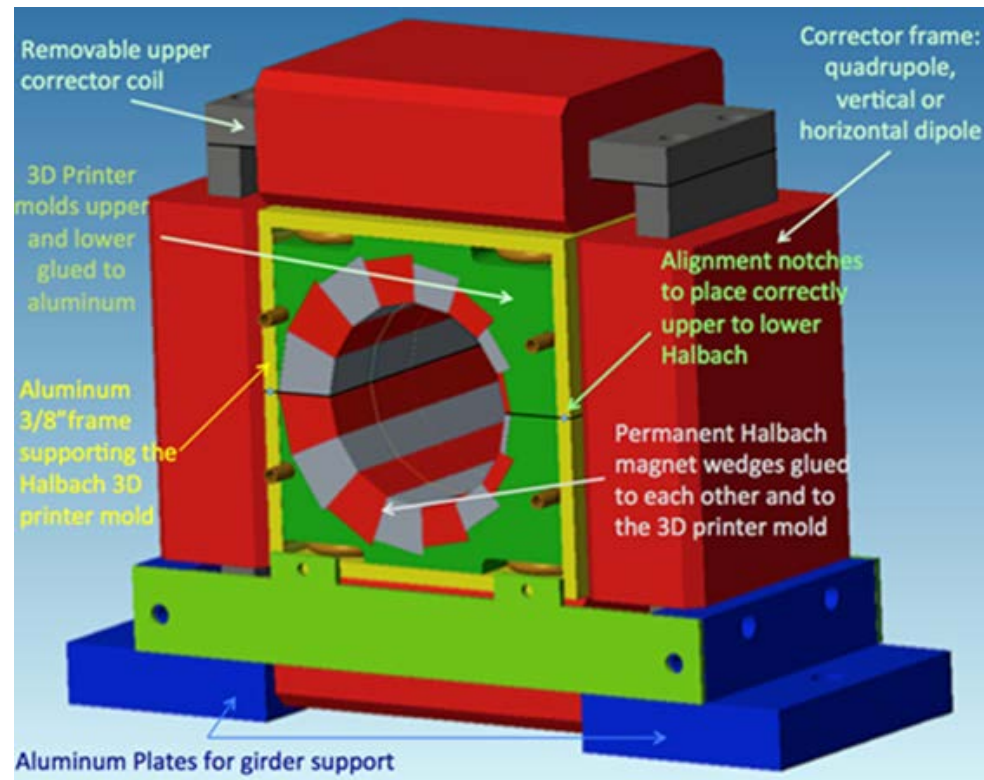
Define Trbojevic/Tsoupis; Design/Fab Mahler/Trabocchi

Quad and dipole corrector gradient and strength

Separate coils for dipole and quadrupole

Skew Quad?

Power Supply interface



# 1<sup>st</sup> Girders Priorities

Build and magnetically measure 8 preproduction halbach magnets w/8 correctors

1. Interface w/Cornell vac. group on vacuum chamber Yulin

Ion pump and NEG (horizontal)

2. BPM configuration Michnoff

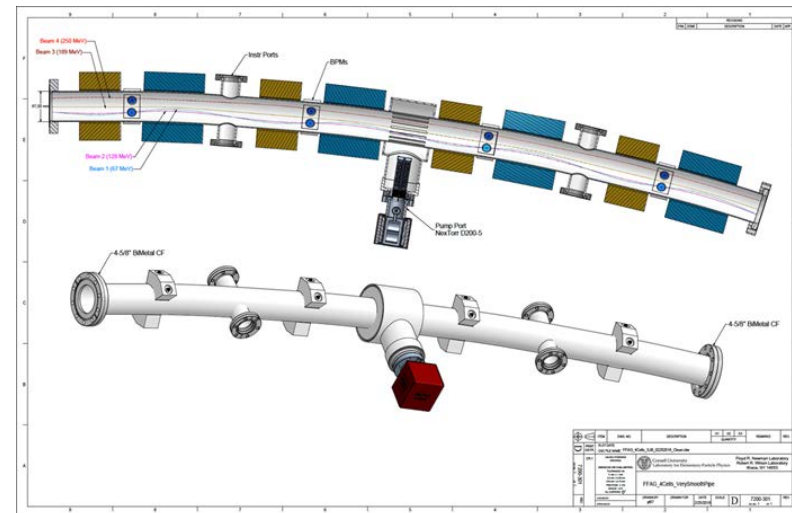
3. Define and design table top Mahler/Trabocchi

Alignment specifications

Magnet mounts – hard pins/frame driven, shim and pin, jacking screws?

Magnet mounts – separate mounts for Halbach and Corrector?

4. Stand design

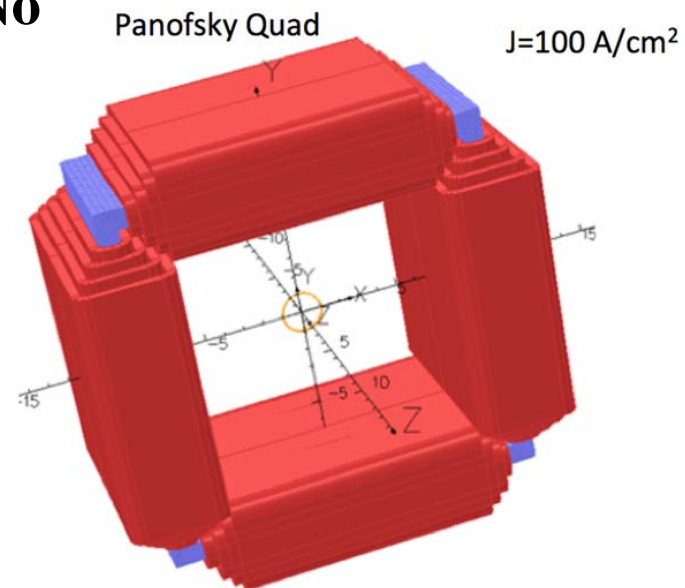


# Halbach Production Plan

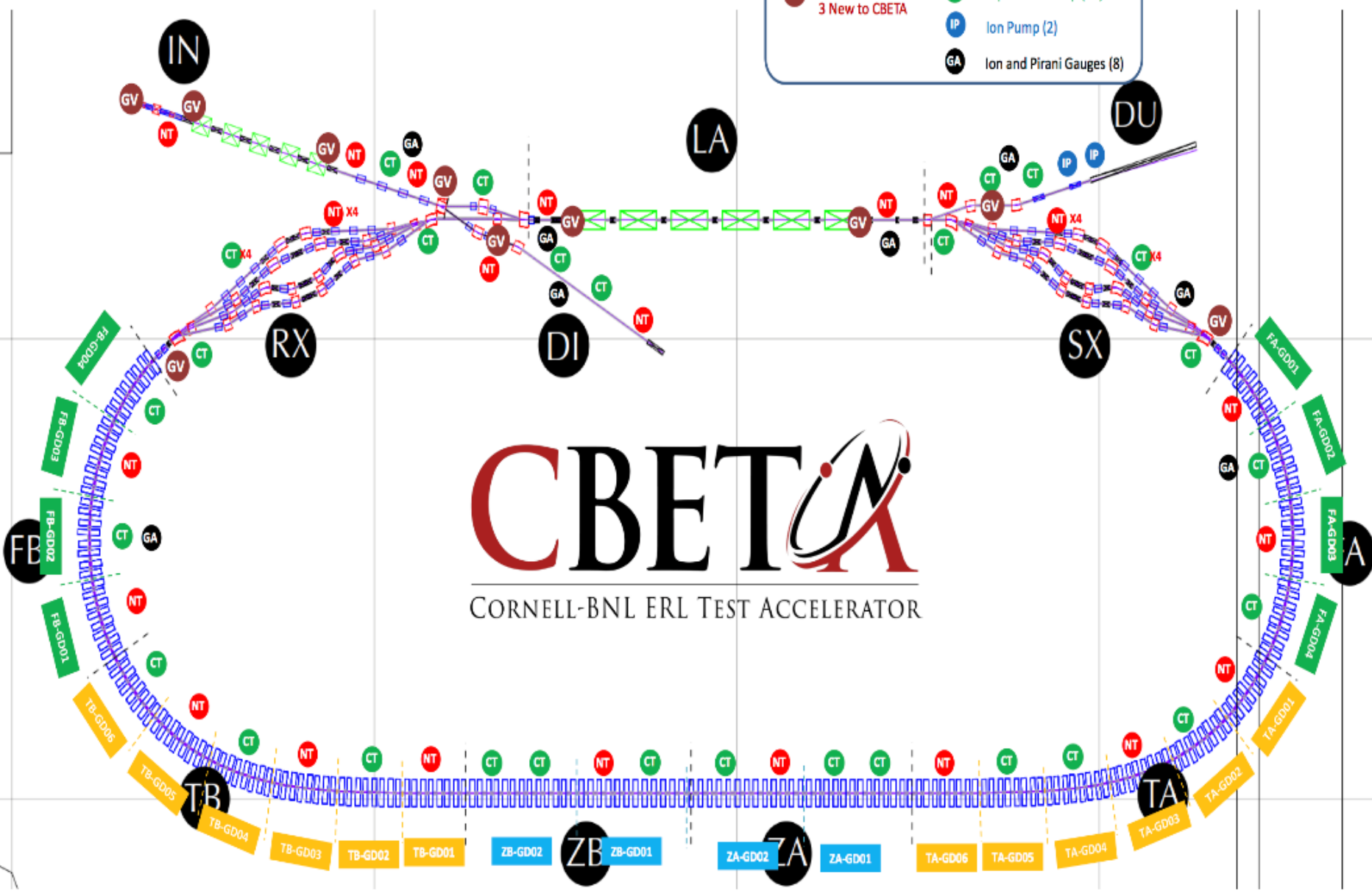
- PMM block dimensions (tolerance), field strength (tolerance), field direction (tolerance). Document design list or drawing or specification
- Temperature stabilization specifications (+/- 5C ??)
- Split magnet frame fabrication method and deflection analysis.

Corrector details:

- Alternating horizontal and vertical corrections? **Yes** QF and QD
- Will BD and QF correctors be the same, interchangeable? **Yes**
- Quadrupole correction on all? **Yes** Skew quad? **No**
- **Are there a chosen power supplies?**
- **Has the method for winding for dipole field and quadrupole field been defined?**
- **Are separate windings needed?**



|           |                  |           |                           |
|-----------|------------------|-----------|---------------------------|
| <b>GV</b> | Gate Valves (11) | <b>NT</b> | NexTorr Pump (28)         |
|           | 10 RF shielded   | <b>CT</b> | CapaciTorr Pump (34)      |
|           | 3 New to CBETA   | <b>IP</b> | Ion Pump (2)              |
|           |                  | <b>GA</b> | Ion and Pirani Gauges (8) |



# CBETA

CORNELL-BNL ERL TEST ACCELERATOR

# **Power Supplies for Correctors**

Calculations by N. Tsoupas



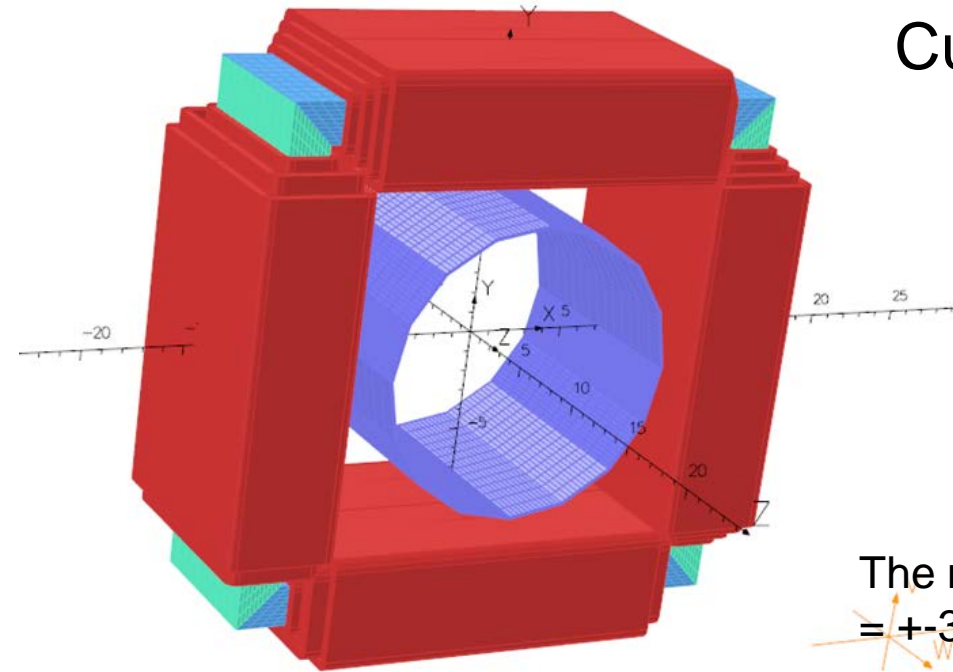
## 3D Calculations

Length of Iron along beam direction=8cm

Inner aperture of WINDOW-frame=10.7 cm

Current Density in coil =1 A/mm<sup>2</sup>

Total Coil Width of coil=1.8 cm



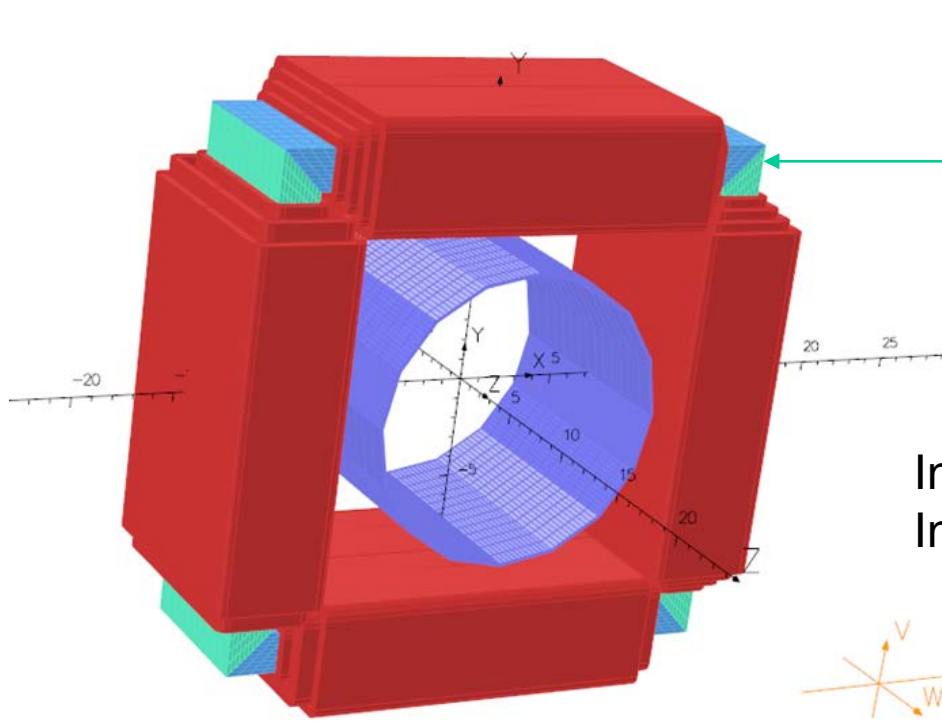
The magnet provides an integral quadrupole field  
=  $\pm 365$  Gauss

The integrated field of the FFAG quadrupole is

$10\text{T/m} \cdot 12\text{cm} = 10\text{T/m} \cdot 0.12\text{m} = 100000 \cdot 0.12 \text{ Gauss} = 12000 \text{ Gauss}$ .

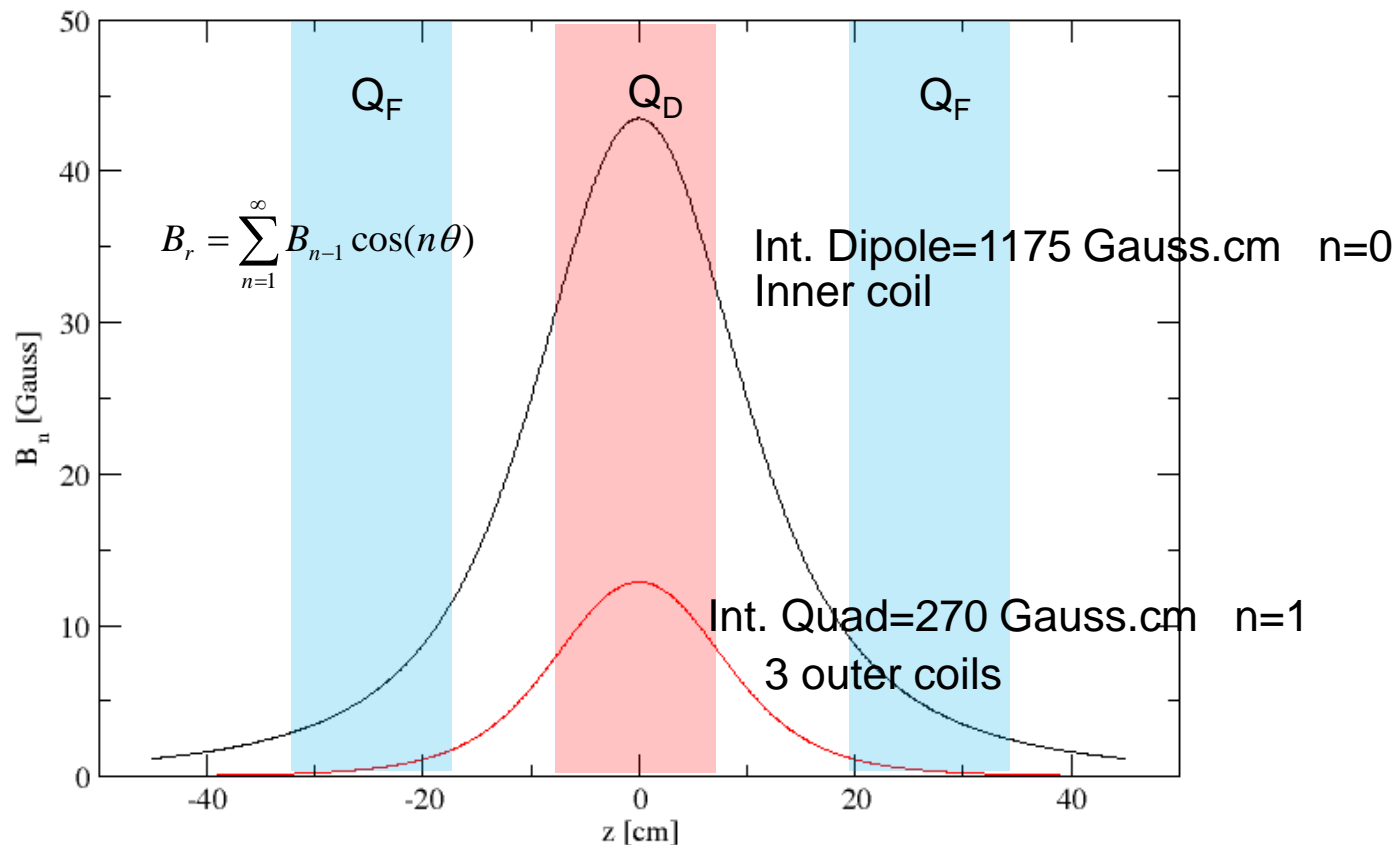
The  $\pm 2\%$  corrector should have an integral quadrupole field =  $\pm 240$  Gauss

Field inside iron <400 Gauss



Integrated Quad=365 Gauss  
Insignificantly small other multipoles

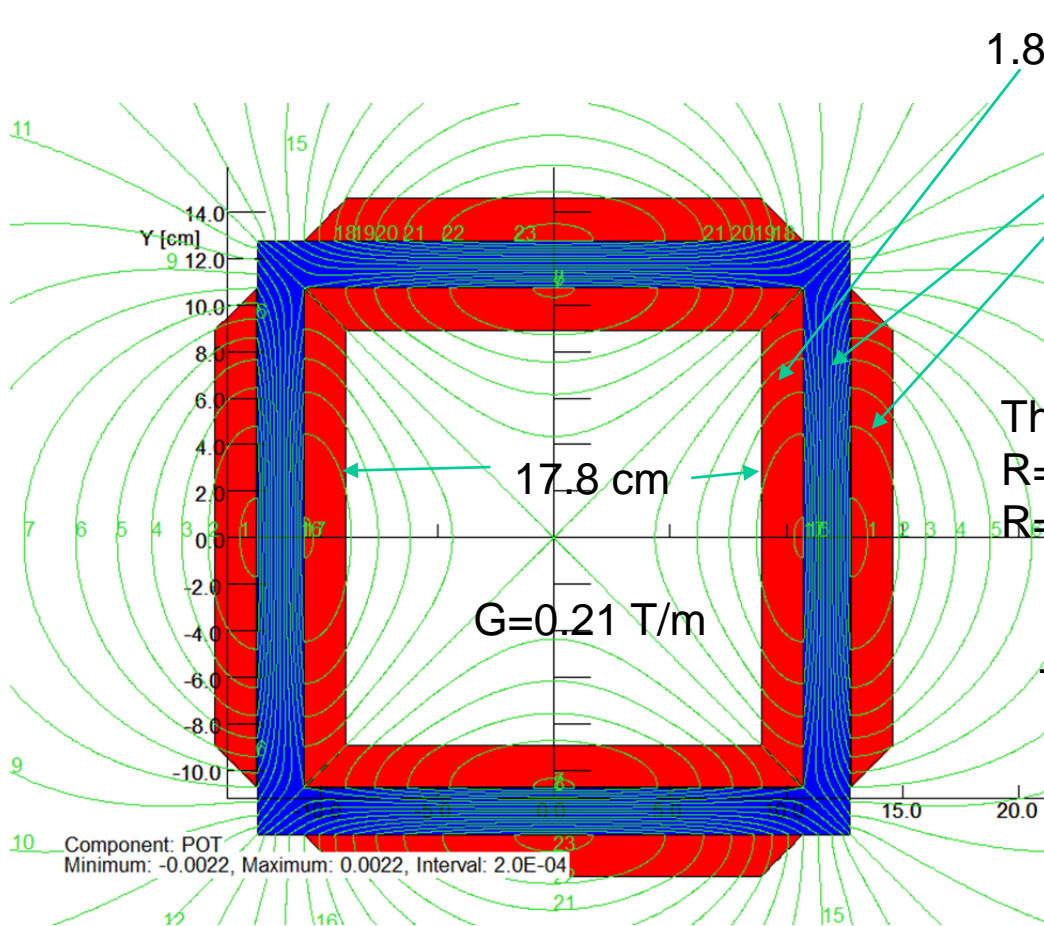
## Multipoles from the correctors at R=1 cm



| Correctors      | Coil connection   | Int. Dipole<br>[Gauss.cm] | Int. N-Quad<br>[Gauss.cm] | J<br>[A/mm <sup>2</sup> ] |
|-----------------|---|---------------------------|---------------------------|---------------------------|
| N-Quad+N-Dipole | Right-Inner-coil + Left-Inner-coil for N-Dipole<br>Three-outer-coils from (R, L, T, B) for N-Quad | 1200 (Normal)             | 275                       | 1.0                       |
| N-Quad+S-Dipole | Top-Inner-coil + Bottom-Inner-coil for N-Dipole<br>Three-outer-coils from (R, L, T, B) for N-Quad | 1200 (Skew)               | 275                       | 1.0                       |

| wire Gauge | Wire Cross Sect [mm <sup>2</sup> ] | Area [mm <sup>2</sup> ] | Number of wires | Length of Magnet Iron [cm] | Length of wire per turn [m] | Total length of wire per coil [m] | Resistance of coper wire per coil [Ohm] | Current in wire [A] | Voltage across Quad-coil 4-coils [V] | Voltage across Dipole-coil 2-coils [V] | Quad-Power [W] | Dipole-Power [W] | Inductance [H] |
|------------|------------------------------------|-------------------------|-----------------|----------------------------|-----------------------------|-----------------------------------|---|---------------------|--------------------------------------|--|----------------|------------------|----------------|
| 14         | 2.08                               | 3528                    | 1696            | 8                          | 0.25                        | 424.04                            | 3.42                                    | 2.08                | 28.50                                | 14.25                                  | 59.27          | 29.64            | 0.0800         |
| 11         | 4.17                               | 3528                    | 846             | 8                          | 0.25                        | 211.51                            | 0.85                                    | 4.17                | 14.21                                | 7.11                                   | 59.27          | 29.64            | 0.0199         |
| 9          | 6.63                               | 3528                    | 532             | 8                          | 0.25                        | 133.03                            | 0.34                                    | 6.63                | 8.94                                 | 4.47                                   | 59.27          | 29.64            | 0.0079         |

THE RESISTANCE DOES NOT INCLUDE THE RESISTANCE OF THE WIRES FROM THE POWER SUPPLY TO THE MAGNET.



In this area ~18mmx196 mm will be 1696 #14 AWG wires.

The magnet iron is ~8cm.

The length of each wire turn is ~25 cm.

The length of the wire in each of the four coils is  $L=25\text{cm} \times 1696=425\text{ m}$ .

The resistance of each coil is:

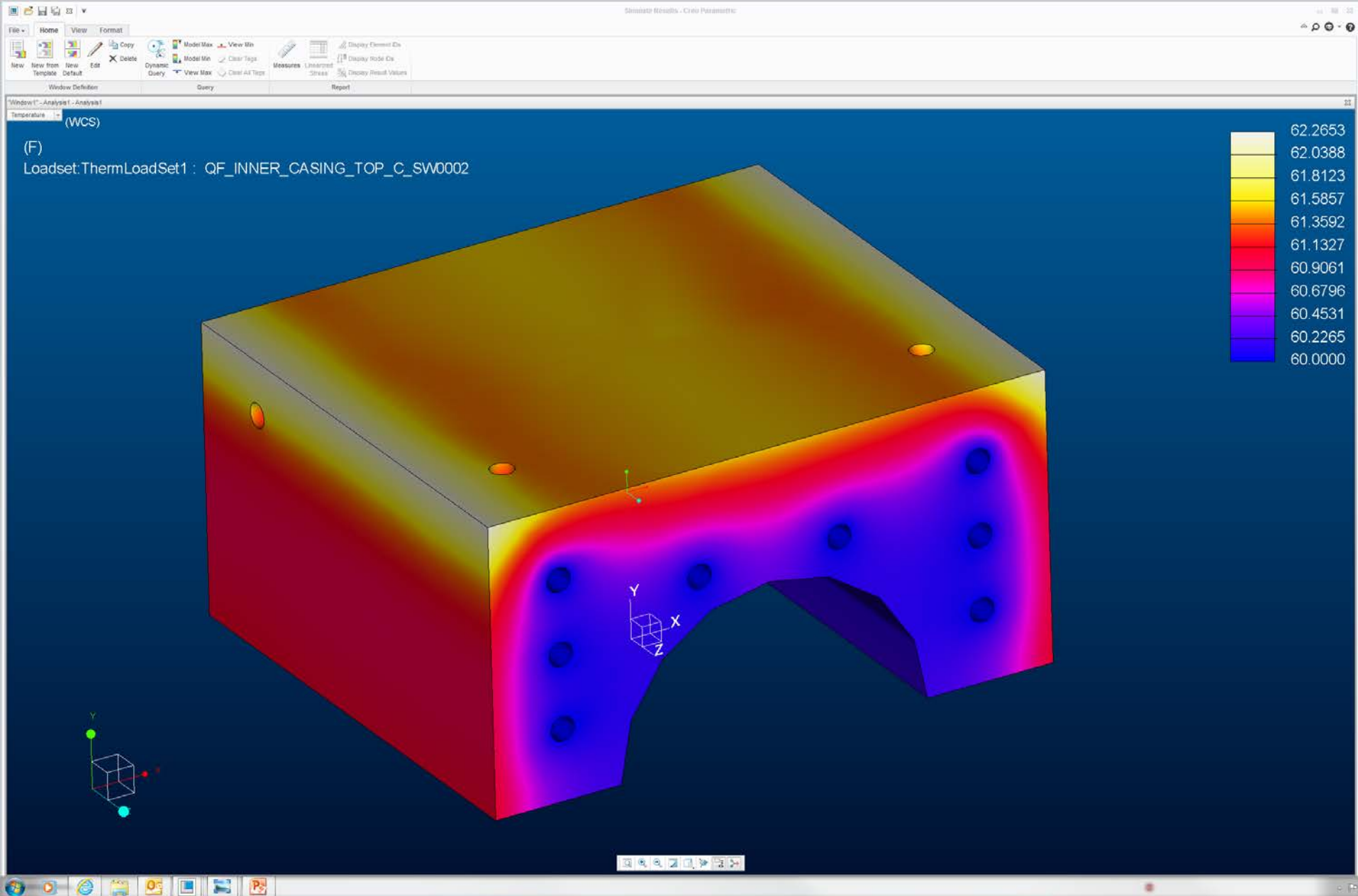
$$R = \rho \cdot (L / \text{Area}) = 1.68 \times 10^{-8} (425 / 2.08 \times 10^{-6}) \text{ Ohm}$$
$$R = 3.4 \text{ Ohm}$$

The current per wire  $I=2.08\text{A}$

The voltage for Quad Corr  $= I \cdot (4 \cdot R) \sim 28.5\text{ V}$

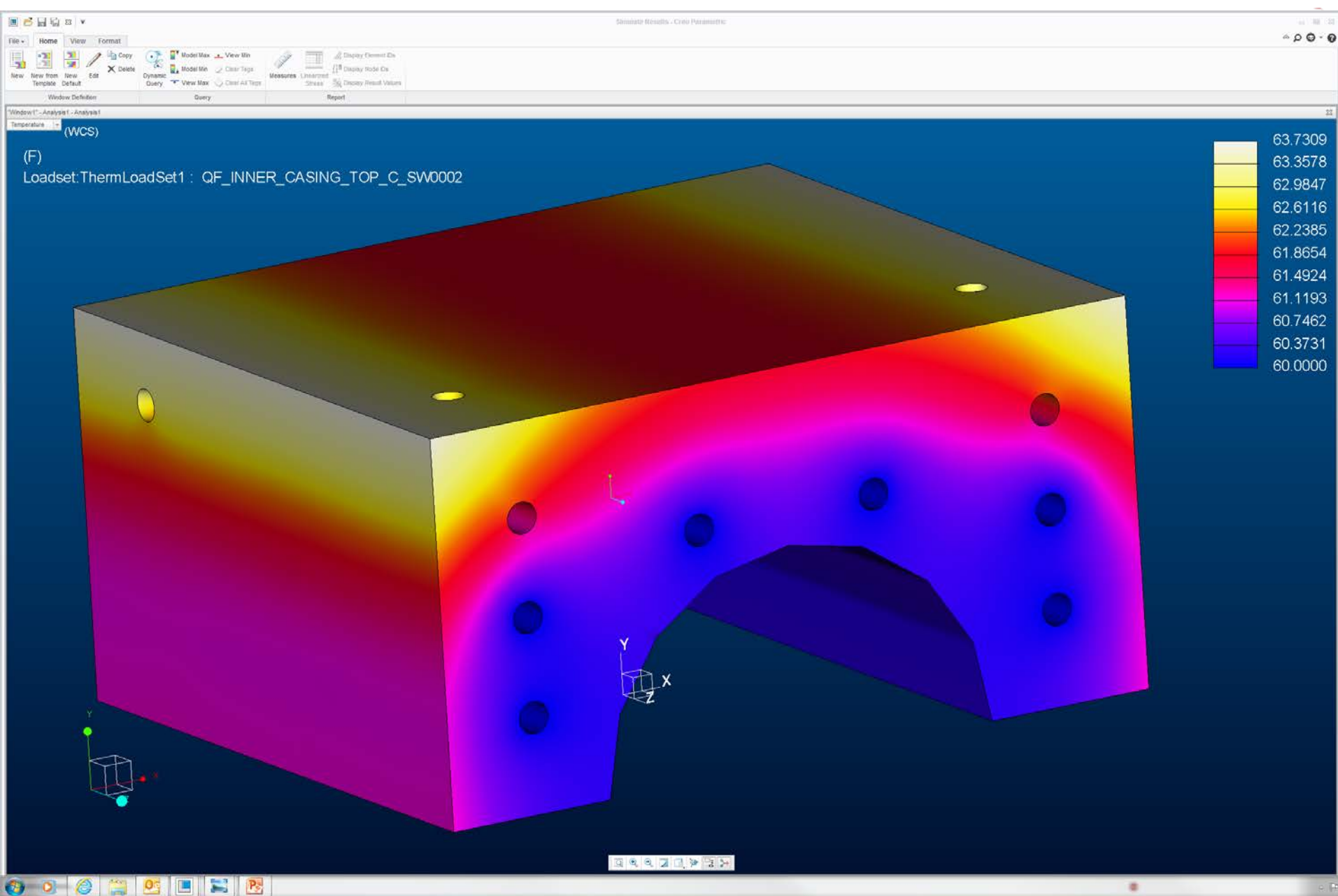
Total Power/cm in four coils ~6.5 W/cm

- Split magnet designs
- G. Mahler

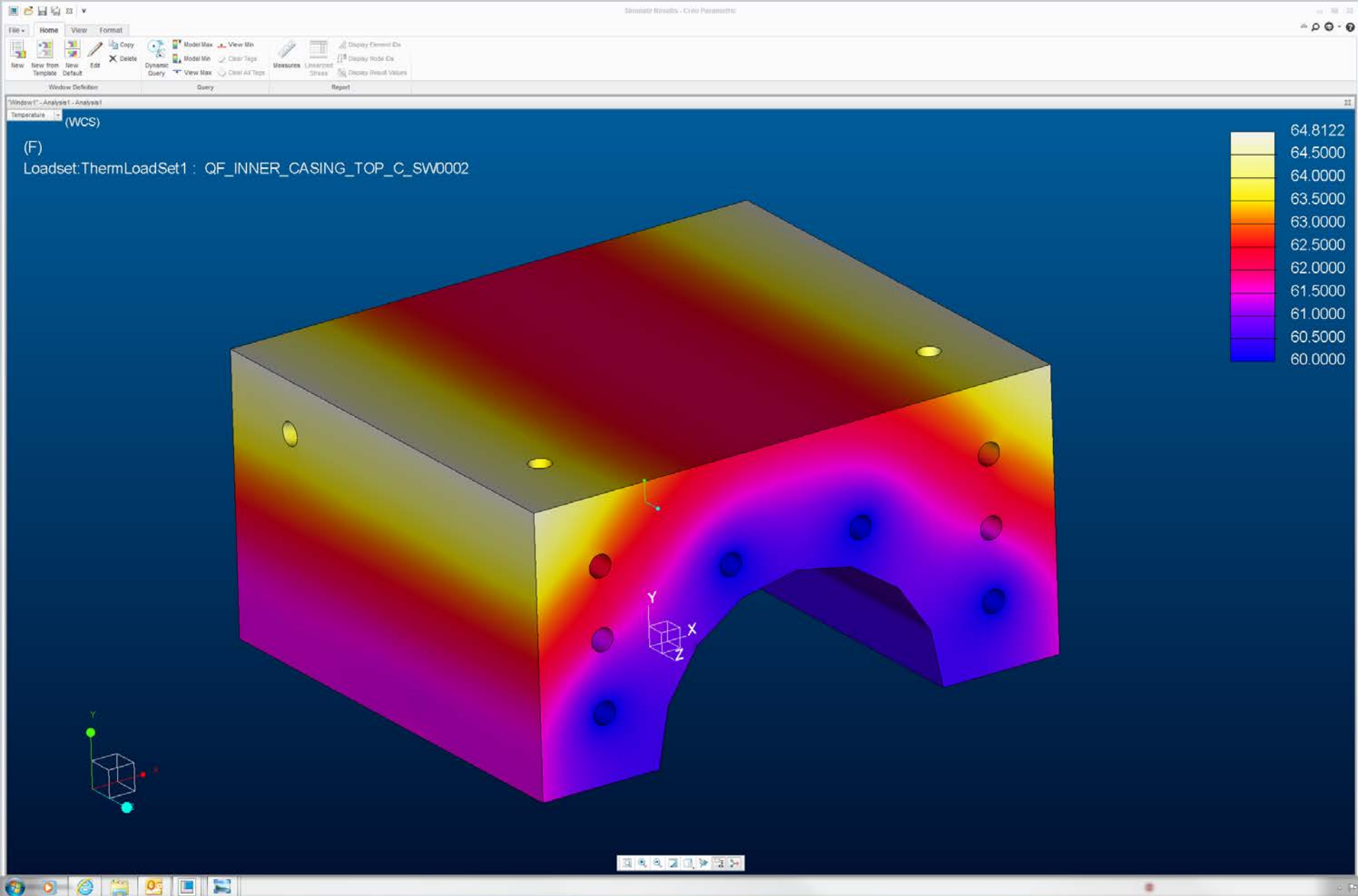


60 F water temp, 5 W/m<sup>2</sup> convection coefficient, 100 Watts top, 50 Watts each side





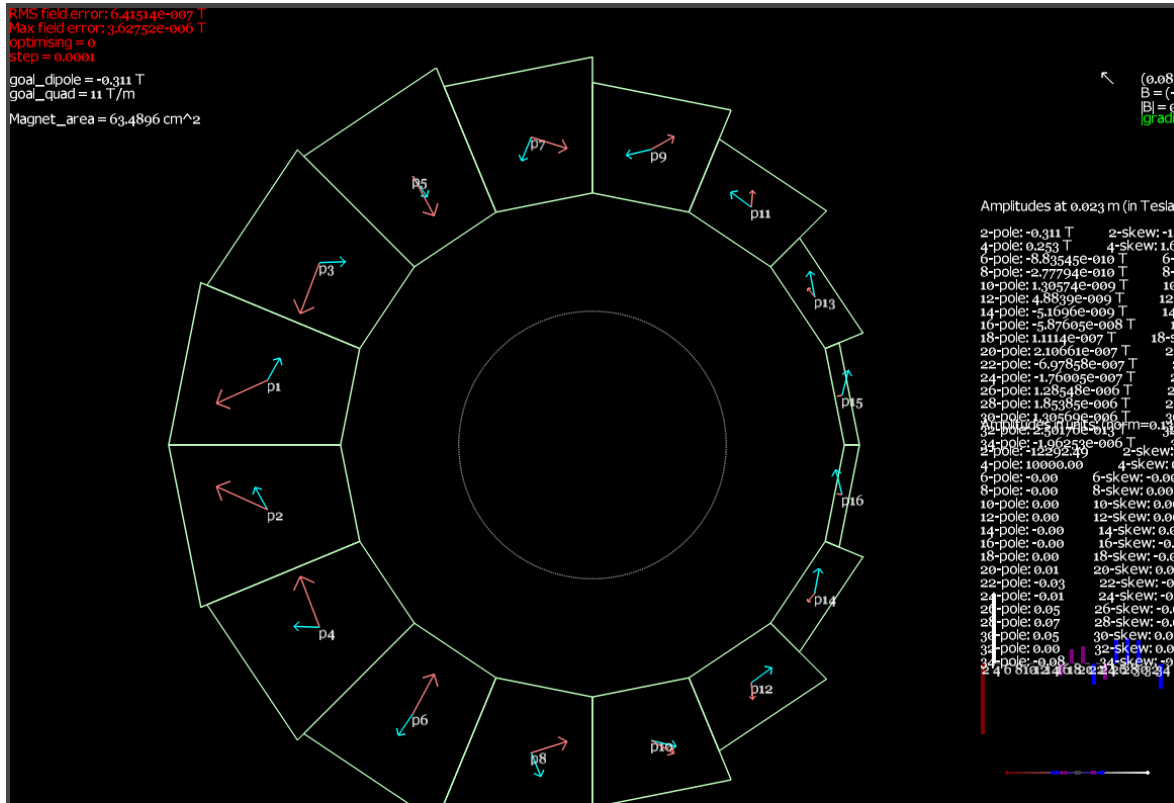
60 F water temp, 5 W/m<sup>2</sup> convection coefficient, 100 Watts top, 50 Watts each side

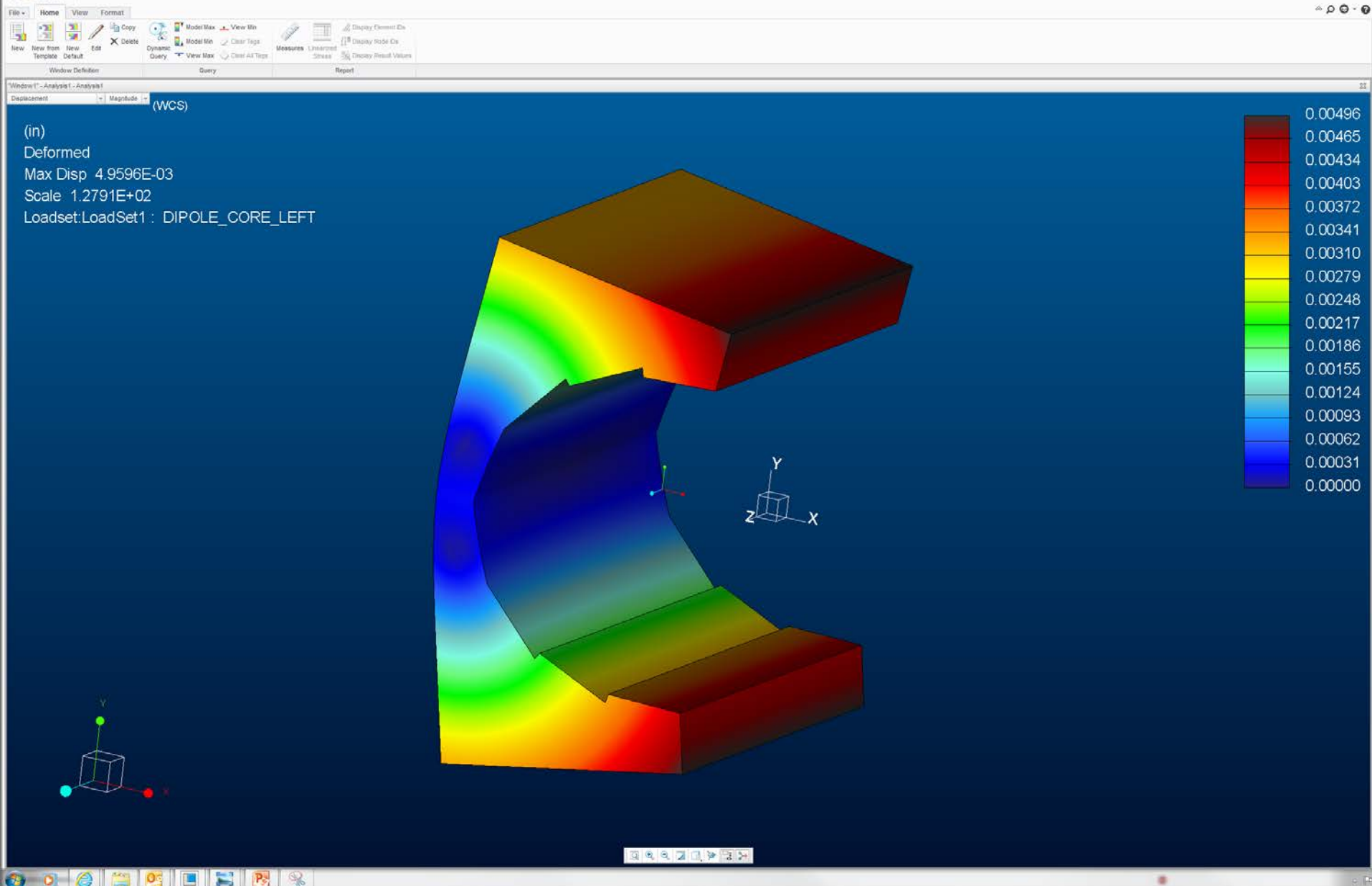


60 F water temp, 5 W/m<sup>2</sup> convection coefficient, 100 Watts top, 50 Watts each side

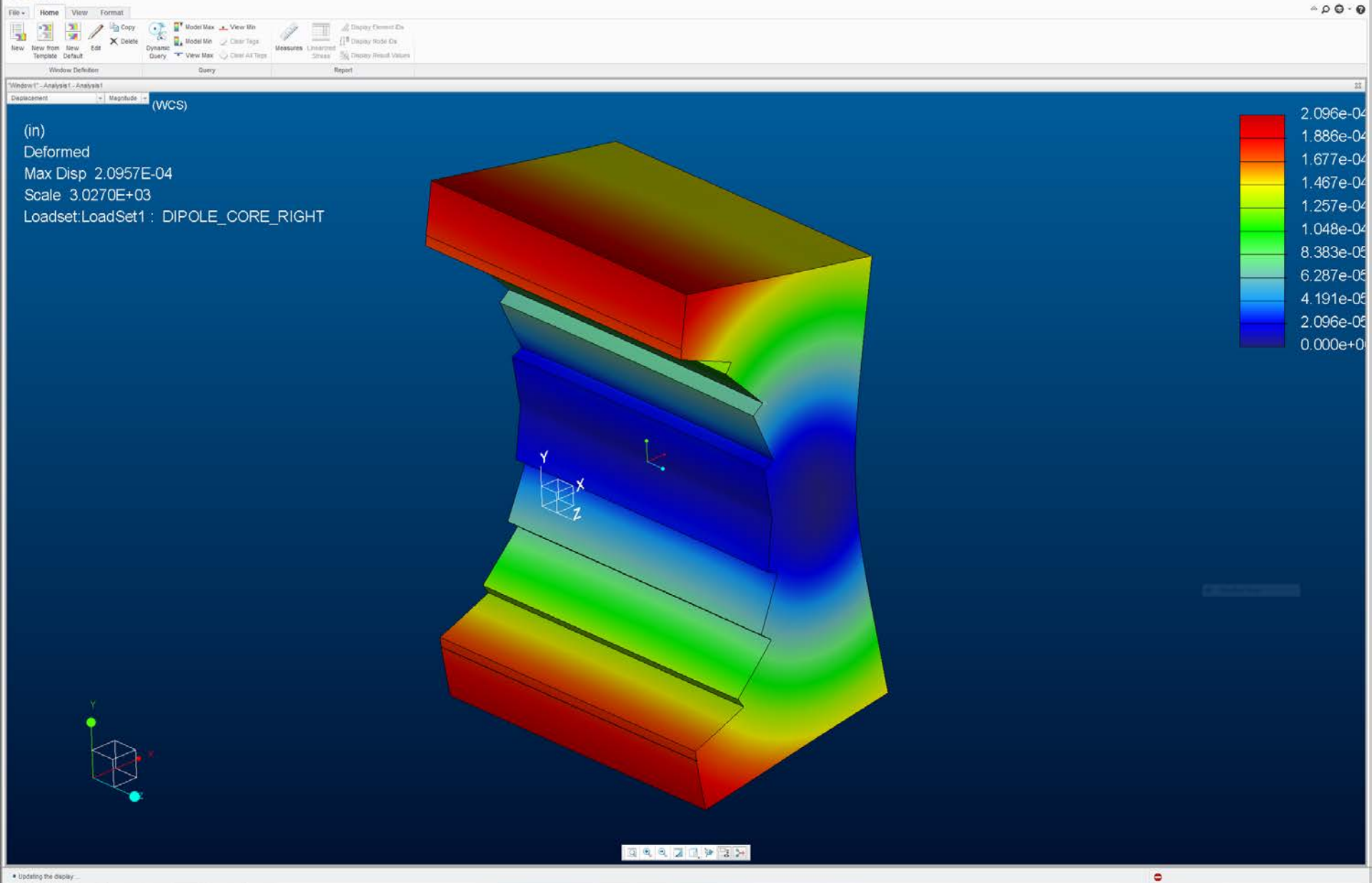
Sheet1

| Piece       | Fx (N/m)    | Fy (N/m)    | Fx (N)      | Fy (N)      | Fx (lbf)    | Fy (lbf) (for nominal length 0.1217m) |
|-------------|-------------|-------------|-------------|-------------|-------------|---------------------------------------|
| p1          | -8763.96633 | -3966.86394 | -1066.5747  | -482.767341 | -239.775531 | -108.530416                           |
| p2          | -8763.96633 | 3966.86394  | -1066.5747  | 482.767341  | -239.775531 | 108.530416                            |
| p3          | -3330.09713 | -8774.88275 | -405.272821 | -1067.90323 | -91.1089545 | -240.074197                           |
| p4          | -3330.09713 | 8774.88275  | -405.272821 | 1067.90323  | -91.1089545 | 240.074197                            |
| p5          | 3695.36607  | -6845.16327 | 449.72605   | -833.05637  | 101.102438  | -187.278522                           |
| p6          | 3695.36607  | 6845.16327  | 449.72605   | 833.05637   | 101.102438  | 187.278522                            |
| p7          | 6136.75709  | -1937.06225 | 746.843338  | -235.740476 | 167.897061  | -52.9965673                           |
| p8          | 6136.75709  | 1937.06225  | 746.843338  | 235.740476  | 167.897061  | 52.9965673                            |
| p9          | 3909.27642  | 2198.57361  | 475.75894   | 267.566408  | 106.954865  | 60.1513214                            |
| p10         | 3909.27642  | -2198.57361 | 475.75894   | -267.566408 | 106.954865  | -60.1513214                           |
| p11         | 240.982639  | 2846.22359  | 29.3275871  | 346.385411  | 6.59310387  | 77.870538                             |
| p12         | 240.982639  | -2846.22359 | 29.3275871  | -346.385411 | 6.59310387  | -77.870538                            |
| p13         | -1170.22008 | 1438.05793  | -142.415783 | 175.011651  | -32.0163417 | 39.3441842                            |
| p14         | -1170.22008 | -1438.05793 | -142.415783 | -175.011651 | -32.0163417 | -39.3441842                           |
| p15         | -806.348861 | -138.855496 | -98.1326563 | -16.8987139 | -22.0610988 | -3.79898202                           |
| p16         | -806.348861 | 138.855496  | -98.1326563 | 16.8987139  | -22.0610988 | 3.79898202                            |
| Top half    | -88.2501751 | -15179.9726 | -10.7400463 | -1847.40266 | -2.41445846 | -415.31264                            |
| Bottom half | -88.2501751 | 15179.9726  | -10.7400463 | 1847.40266  | -2.41445846 | 415.31264                             |

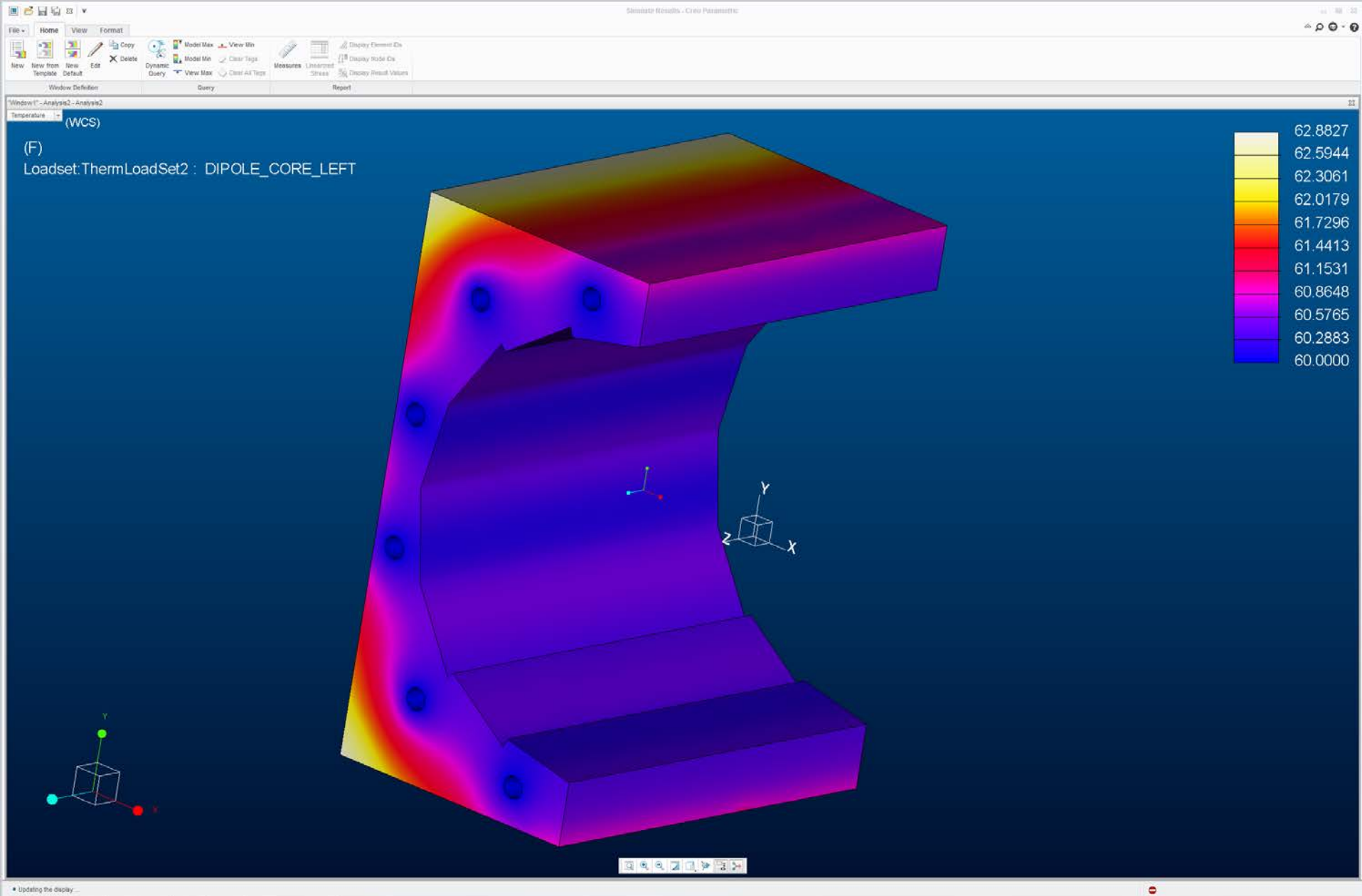




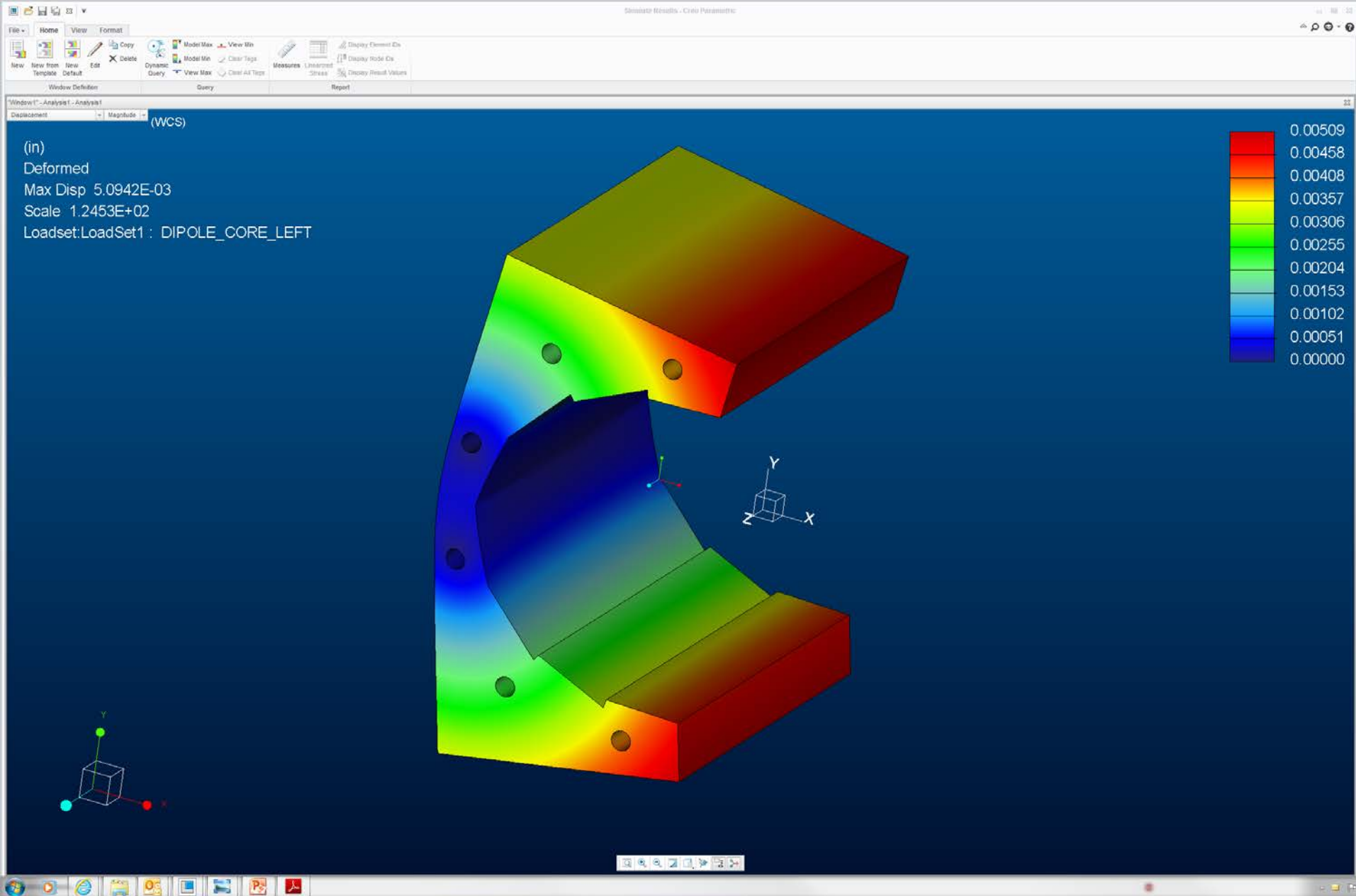
“Left side”



“right side”



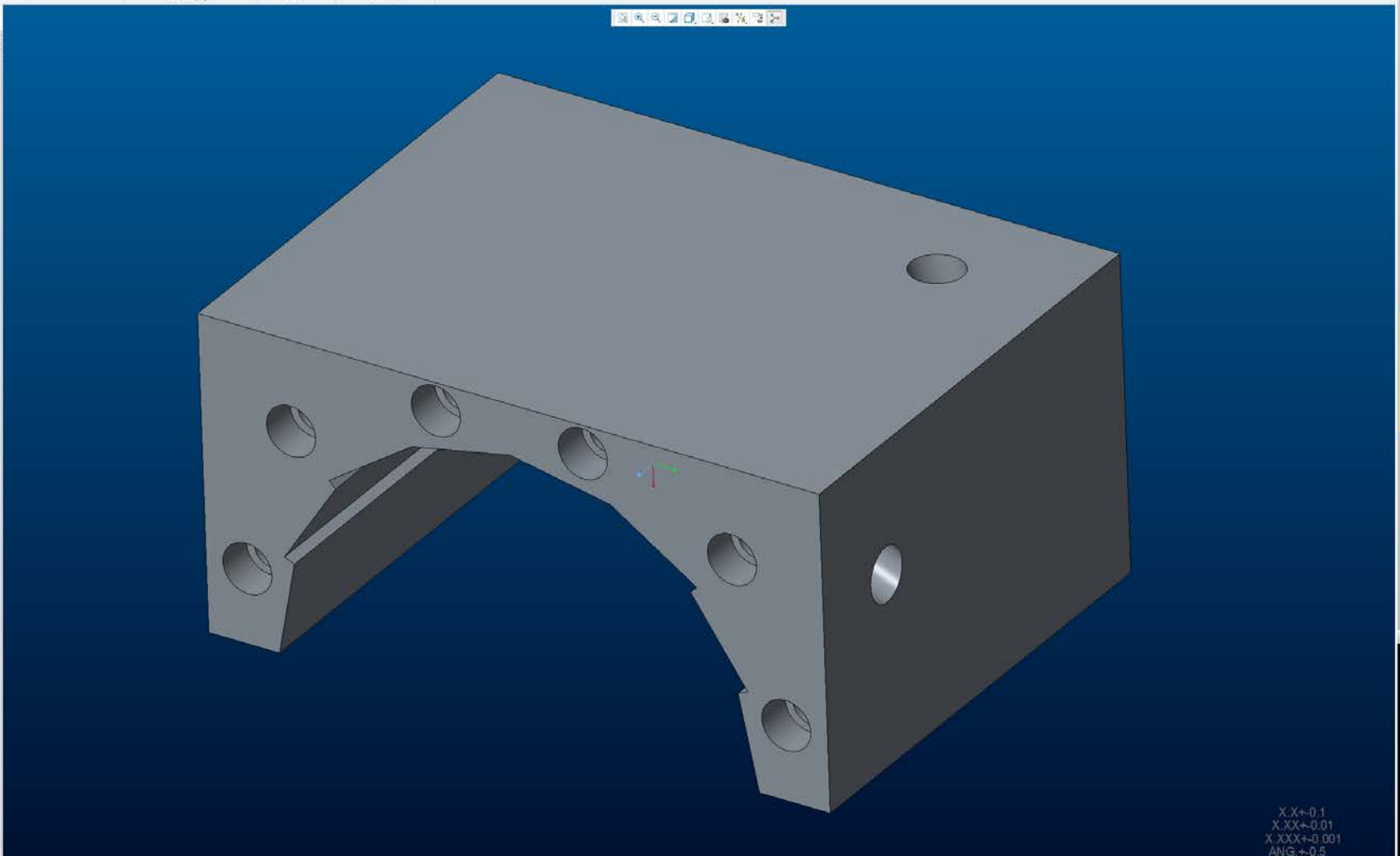
60 F water temp, 5 W/m<sup>2</sup> convection coefficient, 100 Watts top, 50 Watts each side



Slight increase in deflection because of holes

File Model Analysis Annotate Reader Tools View Flexible Modeling Applications  
Layers Hide Show Refr Zoom Out Zoom In Pan Zoom  
Save Orientations Standard Orientation Previous Appearance Gallery Section Manage Views Display Style Activate Close Windows  
Visibility Orientation Model Display Show Window

- Model Tree
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  - Extrude 11
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  - Mirror 2
  - Extrude 19
  - Mirror 3
  - Extrude 20
  - DTM1
  - DTM2
  - Mirror 4
  - Extrude 21
  - Mirror 5
  - Mirror 6
  - Mirror 7
  - Mirror 8
  - Mirror 9
  - Mirror 10
  - Extrude 22
  - Mirror 11
  - Mirror 12
  - Mirror 13
  - Hole 1
  - Mirror 14
  - Mirror 15
  - Mirror 16
  - Hole 2
  - Mirror 17
  - Mirror 18
  - Mirror 19
  - Hole 3
  - Mirror 20
  - Mirror 21
  - Mirror 22
  - Extrude 23
  - Extrude 24
  - Mirror 25
  - Extrude 25
  - DTM4
  - DTM5
  - Extrude 26
  - Mirror 24
  - Extrude 27
  - Hole 4
  - A.11
  - DTM6
  - Extrude 28
  - Hole 5
  - Pu10
  - Mirror 25
  - Mirror 26
  - DTM8
  - Extrude 29
  - Hole 6
  - Pu11
  - DTM9
  - Extrude 30
  - Hole 7
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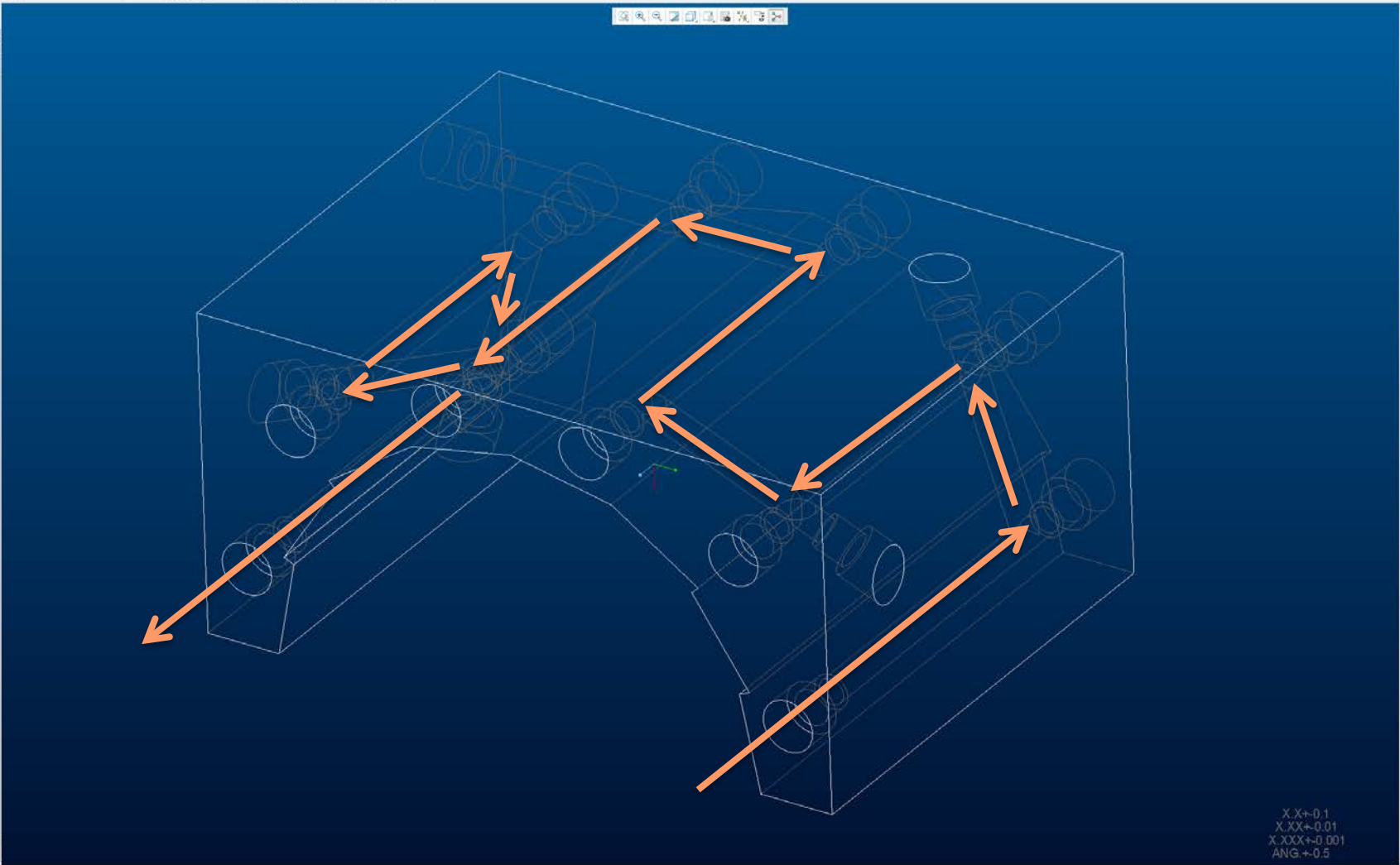


X.X+-0.1  
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File Model Analysis Annotate Render Tools View Flexible Modeling Applications  
Layers Hide Unhide Refr Zoom In Zoom Out Save Operations Standard Orientation Previous Appearance Section Manage Display Style Activate Close Windows  
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- Model Tree
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  - Mirror 2
  - Extrude 20
  - DTM1
  - DTM2
  - Mirror 2
  - Extrude 21
  - Mirror 6
  - Mirror 7
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  - Mirror 10
  - Extrude 22
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  - Hole 1
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  - Extrude 23
  - Extrude 24
  - Mirror 25
  - Extrude 25
  - DTM4
  - DTM5
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  - DTM6
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  - Mirror 25
  - Mirror 26
  - DTM8
  - Extrude 29
  - Hole 6
  - Part1
  - DTM9
  - Extrude 30
  - Hole 7
  - Mirror 27
  - Insert Here



File Model Analysis Annotate Render Manikin Tools View Applications Framework

Home View Pan Zoom Out Zoom In Pan Zoom

Layers Visibility

Save Orientations Standard Orientation Previous

Manage Views Section Appearance Gallery

Exploded View

Display Style

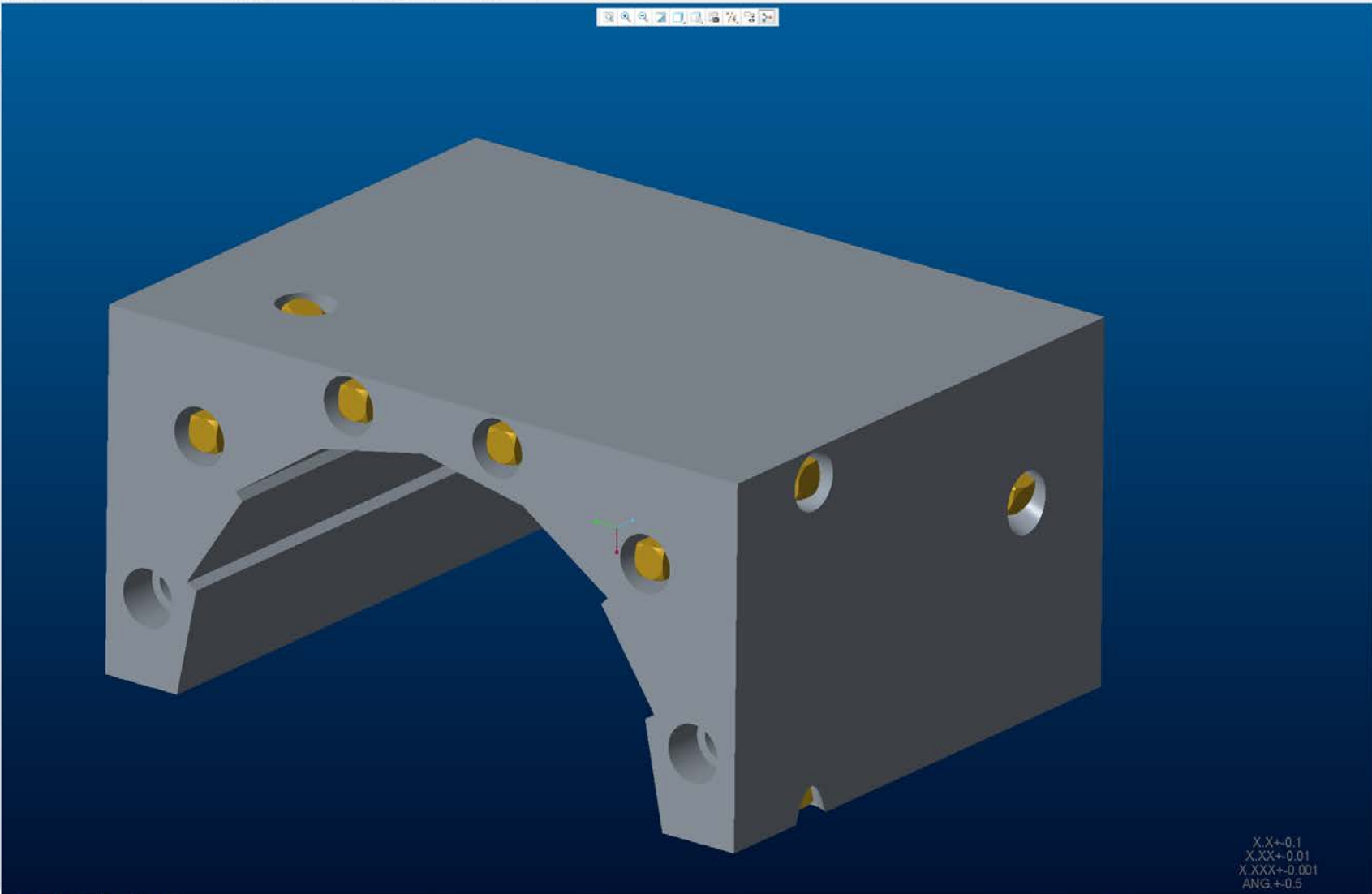
Activate Close Windows

Orientation Model Display Show Window

Model Tree

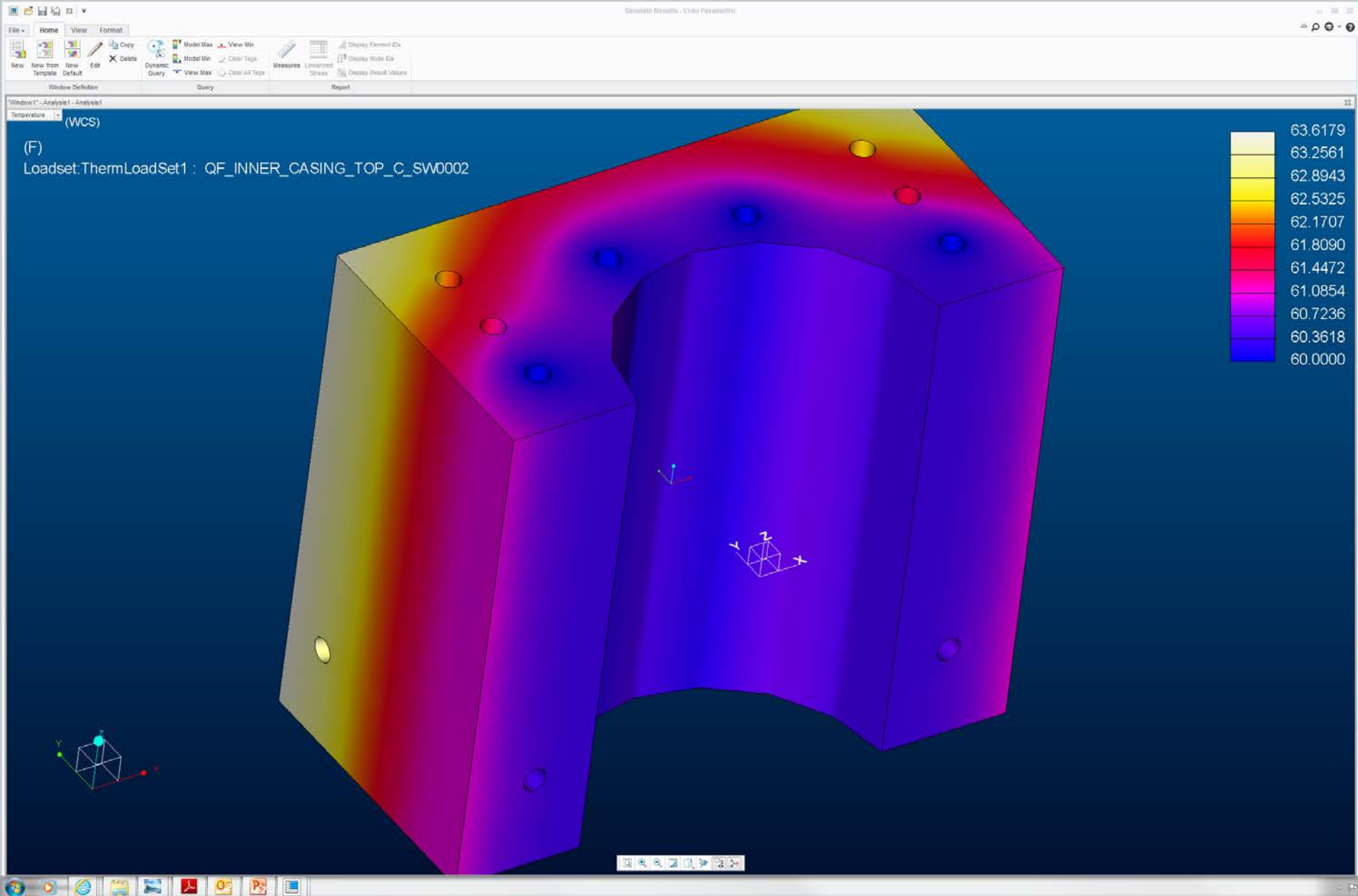
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- DPOLE\_W\_FLUGS.A
- DPOLE\_CORR\_1
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X.X+-0.1  
 X.XX+-0.01  
 X.XXX+-0.001  
 ANG +/-0.5

Windows taskbar showing icons for Internet Explorer, Firefox, Microsoft Office Word, Microsoft Office PowerPoint, and Microsoft Office Excel.



60 F water temp, 5 W/m<sup>2</sup> convection coefficient, 75 Watts top, 37.5 Watts each side